

# Valorization of an Inorganic Industrial Waste for Manufacturing Sulfur Polymer Cement

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## INTRODUCTION

Phosphogypsum (PG),  $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$ , is a by-product coming from the processing of fluoroapatite, phosphate rock, resulting in  $\text{H}_3\text{PO}_4$  production. Phosphate rocks contain high concentrations of some metals and natural radionuclides from  $^{238}\text{U}$  decay-series, in secular equilibrium, which are about 50 times higher than the ones in typical soils. During the industrial process a fractionation of radioelements contained in phosphate rocks is produced. Only the 15 % of the worldwide PG production is recycled (Garg & Jain, 2010). The 85 % of remaining is deposited without any treatment in regulated stacks, and it may have a negative impact on the environment. On the other hand, sulfur polymer cement (SPC) is a civil engineering material, that have recently emerged as stabilizing agent for various waste (López et al., 2011). This paper is focused on the valorization of phosphogypsum in a sulfur polymer cement.

## EXPERIMENTAL

SPC samples were obtained by a mix of different proportions of phosphogypsum, sulfur, gravel, sand and a thermoplastic material used as modified sulfur containing polymer (Table 1). The SPC samples were manufactured according to López et al. (2011). Each sample was called as SPC X-Y where "X" and "Y" are the percentage % wt of elemental sulfur and PG in the mixtures respectively. Morphology and microstructural characterization of samples were performed in a Hitachi S2100 scanning electron microscope (SEM).

The mechanical properties of the SPCs samples cured at ambient temperature for 1 day of age, were measured according to UNE 196-1:2005 standard.

The radioactive characterization was carried out by using a gamma spectrometry system with a XtRa coaxial germanium detector (Canberra). The detector was coupled to a conventional electronic chain, including a multichannel analyser and was shielded with Fe 15 cm thick. The method to measure the radon potential and the emanation factors is described by López-Coto et al. (2009).

The equation of radon conservation in the building material has allowed us to develop a 3D model of diffusive transport in porous media. This model has been solved for two geometries: a block of  $0.04 \times 0.04 \times 0.16 \text{ m}^3$  and a plate of  $1 \times 1 \times 0.04 \text{ m}^3$ , using a numerical algorithm based on finite elements on an unstructured tetrahedral mesh.

Knowing the exhalation rate of the building materials used to construct a specific room, it is possible by modelling to estimate the expected radon concentration in this room under certain ventilation conditions. In this sense, it has been applied a simple model of radon accumulation in a standard room of  $5 \times 5 \times 2 \text{ m}^3$  coated on all sides by plates of the same material.

## RESULTS AND DISCUSSION

The morphology appearance of the surface crack of PG-SPC samples is shown in Fig. 1. The plasticized sulfur covers homogeneously the rounded grains of arid and laminar crystals of

phosphogypsum, formatting a solid matrix with low porosity (Fig. 1).

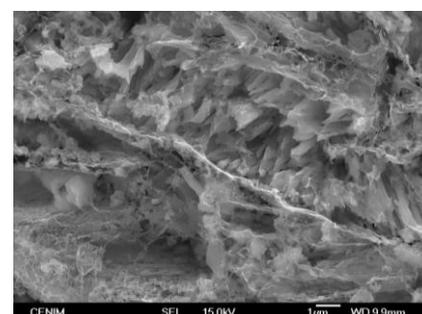


fig 1. SEM image of particles PG bonding from the plasticized sulfur in SPC 26-40 sample.

The compressive strength of the PG-SPC has a value between 49 and 62 MPa, and it is function of the PG content. The  $C_s$  values are similar to the SPC reference (58 MPa).

Table 2 shows the radionuclide concentration of PG and SPC samples. The radionuclides with the highest activity concentration in the SPC samples are  $^{226}\text{Ra}$  (and its daughters of small half live:  $^{222}\text{Rn}$ ,  $^{218}\text{Pb}$ ,  $^{218}\text{Bi}$ ,  $^{214}\text{Pb}$ ,  $^{214}\text{Bi}$ , etc.) and  $^{40}\text{K}$ . There is a good linear correlation between PG added and the activity concentration of  $^{226}\text{Ra}$  ( $y=5.49 + 8.25 R^2=0,9988$ ). To the PG value of  $x=0\%$ , the activity concentration obtained is very low, around  $8 \text{ Bq} \cdot \text{kg}^{-1}$  of  $^{226}\text{Ra}$ , similar to  $^{226}\text{Ra}$  activity concentration in SPC 21-0. If we consider  $x=100\%$ , pure PG, it is obtained an activity concentration for  $^{226}\text{Ra}$  of  $557 \text{ Bq} \cdot \text{kg}^{-1}$ , value very similar to indicated in Table 2 for PG sample, 589

Samples	Sulfur (S)	Gravel	Sand	PG	STX™	S/PG
SPC 21-0*	21.0	23.1	46.1	0.0	2.1	0.00
SPC 17-10	17.0	23.8	47.5	10.0	1.7	1.70
SPC 19-20	19.0	19.7	39.4	20.0	1.9	0.95
SPC 21-30	21.0	15.6	31.3	30.0	2.1	0.70
SPC 26-40	26.0	10.5	20.9	40.0	2.6	0.65
SPC 30-50	30.0	5.7	11.3	50.0	3.0	0.60

Table 1. Composition of SPC samples (%wt.) and sulfur/PG ratios. Gravel/sand=0.5; Sulfur/STX™=10\*Calcium carbonate (99.5% purity Panreac) in substitution of PG.

**palabras clave:** Fosfoyeso, Radón, Microencapsulación, Cementos Poliméricos de Azufre

**key words:** Phosphogypsum, Radon, Microencapsulation, Sulfur Polymer Concrete

Code	SPC 21-0	SPC 17-10	SPC 19-20	SPC 21-30	SPC 26-40	SPC 30-50	PG
% PG	0	10	20	30	40	50	100
<sup>210</sup> Pb	8.0 ±0.6	70 ±5.0	143 ±9.0	219 ±13.0	264 ±16.0	340 ±20.0	624 ±37.0
<sup>238</sup> U ( <sup>234</sup> Th)	12 ±2.0	21 ±2.0	12 ±2.0	38 ±3.0	50 ±4.0	60 ±4.0	97 ±6.0
<sup>232</sup> Th ( <sup>212</sup> Pb)	9.1 ±0.6	9.4 ±0.7	8.6 ±0.6	8.1 ±0.5	5.9 ±0.4	5.8 ±0.4	8.2 ±1.0
<sup>226</sup> Ra	7.4 ±0.5	63 ±4.0	115 ±7.0	179 ±11.0	226 ±13.0	282 ±17	589 ±34.0
<sup>228</sup> Th	8.8 ±0.8	8.7 ±0.7	<6	6.8 ±0.7	7.3 ±0.6	6.1 ±0.6	7.8 ±0.7
<sup>228</sup> Ra ( <sup>228</sup> Ac)	8.2 ±0.8	8.6 ±0.8	8.8 ±0.8	6.9 ±0.7	<4	<4	8 ±1.0
<sup>40</sup> K	580 ±30.0	528 ±32.0	394 ±24.0	347 ±21	239 ±15.0	143 ±10.0	<18
Index	0.26	0.43	0.56	0.75	0.85	1.01	2.01

Table 2. Radionuclide concentration of SPC -PG samples and PG (Bqkg<sup>-1</sup>).

Bq·kg<sup>-1</sup>.

The activity concentration index (I) was calculated (Ec. 1):

$$I = \frac{[^{226}\text{Ra}]}{300} + \frac{[^{228}\text{Ra}]}{200} + \frac{[^{40}\text{K}]}{3000} \quad (1)$$

Where [<sup>226</sup>Ra], [<sup>228</sup>Ra], [<sup>40</sup>K] are, respectively, the activity concentrations in the building material considered, expressed in Bq·Kg<sup>-1</sup>. The activity concentration index (I) in the studied samples agrees with the EU references values, in the range 0.3 - 1 mSv·a<sup>-1</sup> (Table 2) (EC, 1999). Only SPC 30-50, with the 50% of PG, presents an I value around 1, so this could not be used in bulk amounts.

It has been carried out by modelling a simulation of a block of polymer cement (SPC 30-50) that emanates through all its sides excepting for the base (0.04x0.16 m<sup>2</sup>). The blocks do not have a uniform radon exhalation rate, showing the geometry effect of this parameter (Fig. 2). In turn, the mean value for radon exhalation throughout its surface in contact with air is 3.6 ± 1.6 Bq·m<sup>-2</sup>·h<sup>-1</sup>, very similar to the

	E	σ	C <sub>Rn</sub> (λ <sub>v</sub> = 2 h <sup>-1</sup> )	C <sub>Rn</sub> (λ <sub>v</sub> = 0.1 h <sup>-1</sup> )
SPC 17-10	4.0	0.5	4	67
SPC 19-20	4.4	0.5	4	74
SPC 21-30	8.7	1.1	8	146
SPC 26-40	7.5	0.9	7	125
SPC 30-50	11.7	1.4	10	196

Table 3. Radon exhalation rate, E (Bq m<sup>-2</sup> h<sup>-1</sup>), of a plate (1x1x0.04 m<sup>3</sup>) and the expected radon concentration, C<sub>R</sub> (Bq·m<sup>-3</sup>), in a standard room.

experimental values ones.

This model was applied to different plates 1x1x0.04 m<sup>3</sup> made off SPC-PG samples, the exhalation rates range from 2 to 12 Bq·m<sup>-2</sup>·h<sup>-1</sup> (Table 4), being of the same order of magnitude or slightly higher of typical building materials (1-10 Bq·m<sup>-2</sup>·h<sup>-1</sup>).

The plate made with SPC 30-50 presents the highest mean values for the exhalation rate, 11.7 ± 1.4 Bq·m<sup>-2</sup>·h<sup>-1</sup>, assuming an exhalation only in one side; it is due to the highest Rn Pot values, 30.6 Bq·kg<sup>-1</sup>. Fig. 3 shows the radon exhalation rates obtained for different surface points of plate SPC 30-50; the highest values are found near the edges of the plate. Thus, the central part of the plate presents a value of 9 Bq·m<sup>-2</sup>·h<sup>-1</sup>, while their edges have values until above 15 Bq·m<sup>-2</sup>·h<sup>-1</sup>.

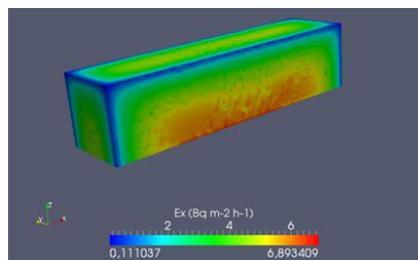


Fig 2. Radon exhalation rate obtained by modelling a specimen of 0.004 x 0.004 x 0.16 m<sup>3</sup> made with SPC 30-50 sample.

The expected radon concentration inside a standard room (5x4x2.5 m<sup>3</sup>) built with the plates (Fig. 3) is presented in Table 3. In the standard room with a good ventilation (air enhance, λ<sub>v</sub> = 2 h<sup>-1</sup>), the highest expected radon concentration is reached inside the room with SPC 30-50, C<sub>Rn</sub>=10 Bq·m<sup>-3</sup>, but this value did not exceed the average radon

concentrations to 200 Bq·m<sup>-3</sup>, reference value in the EU for new houses. Under poor ventilation (λ<sub>v</sub> = 0.1 h<sup>-1</sup>) the average radon concentrations increase. In SPC 30-50 the radon concentration achieved was 196 Bq·m<sup>-3</sup>, very similar to the reference value in the EU, 200 Bq·m<sup>-3</sup>.

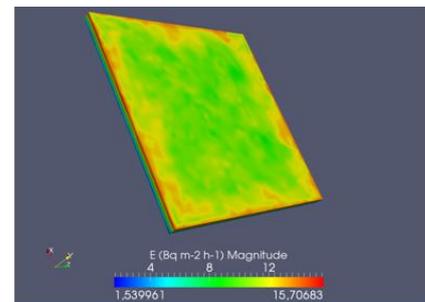


Fig 3. Radon exhalation rate obtained for different surface points of plate (1 x 1 x 0.04 m<sup>3</sup>) of SPC 30-50 samples.

## CONCLUSIONS

SPC permitted the stabilization and solidification of PG with a low radionuclide. The incorporation of PG to the SPC does not significantly change the physical and mechanical properties of SPC when the PG is added in the 10-40% weight range. Activity concentration indices in the SPC-PG samples are lower than reference values. Therefore, these SPC-PGs can be used without radiological restrictions in manufacture building materials.

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