

# Mineralogy, Geochemistry, Petrophysics and Rock Mechanics of the Corvio Sandstone

/ JACOBO CANAL VILA (1), ISMAEL FALCÓN SUÁREZ (2), VICTOR BARRIENTOS RODRÍGUEZ (2), JORDI DELGADO MARTÍN (2,\*)

(1) Fundación Ciudad de la Energía. Avenida Presidente Rodríguez Zapatero s/n. 24492, Cubillos de Sil, León (Spain)

(2) Civil Engineering School. Campus de Elviña s/n. University of A Coruña. 15192, A Coruña (Spain)

## INTRODUCTION.

It is well known that the injection of reactive fluids (like CO<sub>2</sub>) into geological formations trigger a series of interlinked thermo- hydro- chemo- mechanical phenomena (or THCM) affecting the properties of the reservoir, its seals or even the cementitious materials used in wellbores. Because water is always present in the pore space of these rocks, the forced injection of CO<sub>2</sub> (either as liquid, gas or supercritical fluid) induces its acidification and the onset of reactive processes which are especially notorious when carbonate or carbonate-bearing rocks are present. Accompanying CO<sub>2</sub>, the co-injection of subordinated gasses (O<sub>2</sub>, SO<sub>2</sub>...) might exacerbate their reactivity owing the oxidation of reduced mineral phases already present or by promoting an enhanced acidity in the case of the S-bearing gasses.

Petrophysics and rock mechanics provide with an invaluable toolbox with which to assess key rock properties and to elaborate integrated reservoir models. When these techniques are used from a traditional viewpoint, they tend to neglect the crucial importance of the THCM couplings which are inherent, however, to reactive systems.

Core-flooding experiments performed at P-T conditions akin to those *in situ* have a great potential in helping us to unravel complex THCM processes provided that it is feasible the separation of each of their corresponding contributions. To this respect, in the present study we focus on the comprehensive characterization of a reference rock material with a dual purpose: First, as a necessary first step before proceeding with more complex experimental protocols (like reactive fluid injection); and second, to evaluate the adequacy of this material as laboratory standard for petrophysics and rock mechanics studies.

## MATERIALS AND METHODS.

The studied material has the trade name of Corvio Sandstone®. Geologically speaking, this material defines the Corvio Mb which appears as a 20 m thick lithosome at the top section of the Frontada Fm (Campoó Gr; Lower Cretaceous). It is made of siliceous sandstones and conglomerates associated with braided fluvial channels showing dm to m trough-type cross bedding (Hernández et al., 1999).

Four blocks of the Corvio Sandstone (0.3x0.2x0.5 m each; Fig. 1) were used to obtain a total of 228 cylindrical plugs of 38.1 and 50 mm diameter. Additional irregular samples were selected in order to apply a number of physico-chemical characterization techniques: FRX (Bruker-AXS S4 Pioneer), ATD-TG-FTIR (TA Inst. SDT 2690 coupled to Bruker Vector 22), DRX (Siemens D5000), CHNS (ThermoFinnigan FlashEA1112), BET (Micromeritics Gemini VII 2390a), SEM-EDS (JEOL JSM-6400), petrography, He pycnometry (Quantachrome Ultrapyc 1200e), Hg porosimetry (Quantachrome Poremaster-60). With respect the mechanical, petrophysical and hydrodynamic properties our assessment included the measurement of the indirect tensile (Brazilian), unconfined and confined (triaxial) strengths (MTS 815), P- and S- wave velocities, water and gas (N<sub>2</sub>) permeabilities, immersion porosity and dry density. Based on the previous data the static and dynamic elastic moduli, as well as the critical stress states (Hakala et al., 2007) where computed. The characterization of the Corvio Sandstone was complemented with an X-Ray  $\mu$ CT-scan (XRadia MicroXCT-300).

On a general basis, 10 samples were used to assess the statistical significance of the properties determined.



fig 1. Rock blocks of the Corvio Sandstone after core plug extraction.

## RESULTS.

Corvio Sandstone can be classified as a grain-supported quartzarenite with microcrystalline silica cement. The main mineral constituents are quartz (~94 wt. %) with subordinated kaolinite (~3.5 wt. %) and K-feldspar (~1.7 wt. %). Trace amounts of ilmenite (~0.2 wt. %) have been observed in the  $\mu$ CT scans while ~0.5 wt. % of carbonates is inferred from the ATD-TG-FTIR. Quartz grains are typically sub-rounded, well sorted and their average grain size hovers around 0.15-0.3 mm. In the studied samples fossils are reduced to scarce cm-size spots with remnants of vegetal debris (cf. Hernández et al., 2009). Based on ATD-TG-FTIR, the weight % of hydrated minerals is ~0.5 while C, N and S-compounds are below 0.05 wt. %. The average BET specific surface is 1.09±0.07 m<sup>2</sup>/g (n=12) while porosity and dry density are 14.45% (n=224) and 2037 kg/m<sup>3</sup> (n=227). Hg porosimetry shows that pore size spans from 2.5 to

**palabras clave:** Arenisca de Corvio, permeabilidad, resistencia, petrofísica, velocidad de ondas P y S

**key words:** Corvio sandstone, permeability, strength, petrophysics, P- and S- wave velocities

resumen SEM 2013

\* corresponding author: [jdelgado@udc.es](mailto:jdelgado@udc.es)

100  $\mu\text{m}$  while the median is  $\sim 20 \mu\text{m}$ .  $\mu\text{CT}$ -scan data shows that although pores tend to have an equant-shape some of them may be compliant upon loading. This observation is supported by the stress-strain curves obtained.

### Strength and Stress-Strain Behavior.

Geomechanical tests were performed on 50 mm diameter cylindrical plugs prepared to meet the recommendations of the International Society for Rock Mechanics. In the case of the unconfined compression strength (UCS) and triaxial tests, the axial strain was recorded with a dual-averaging, knife-edge type, extensometer while the lateral strain was measured with the aid of a circumferential, chain-type, gage.

The mean tensile strength of the Corvicio Sandstone is  $2.3 \pm 0.14 \text{ MPa}$  ( $n=11$ ) while UCS is  $41.3 \pm 1.0 \text{ MPa}$  ( $n=10$ ). These data were combined with the results obtained in additional drained triaxial tests performed at 5, 10, 30 and 50 MPa which were needed to obtain the full strength envelope (Fig. 2). This was computed following the intact rock Hoek and Brown (1980) criterion (HB), as updated by Hoek *et al.* (2002). Assuming that the parameters  $s$  and  $a$  of the HB model are equal to 1 and 0.5, respectively,  $m_b$  is 15.0. Similarly, application of the linear Mohr-Coulomb criterion provides with an apparent cohesion ( $c$ ) of  $\sim 20 \text{ MPa}$  and a friction angle ( $\phi$ ) of  $28.5^\circ$ .

Taking into account the stress-strain behavior observed in the UCS tests, the static Young modulus ( $E$ ) and Poisson ratio ( $\nu$ ) of the Corvicio Sandstone are  $11.41 \pm 0.35 \text{ GPa}$  and  $0.38 \pm 0.01$ , respectively. In addition, based on the computed volumetric strain and the methods discussed by Nicksiar and Martin (2012), the crack initiation and crack damage stresses occur at  $6.2 \pm 0.2$  and  $26.0 \pm 0.8 \text{ MPa}$ , respectively.

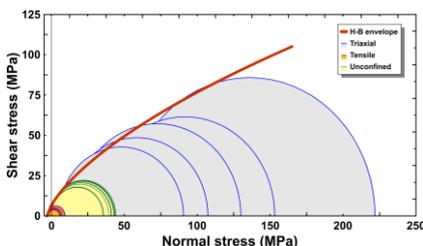


fig 2. Mohr circles corresponding to the different mechanical tests performed (Brazilian, UCS and triaxial) with the Corvicio Sandstone. The computed Hoek-Brown strength envelope computed from these tests is also shown.

### Ultrasonic P- and S-Wave Velocities.

P- and S- wave velocities were measured by applying the time-of-flight technique to cylindrical, 38.1 mm diameter plugs submitted to unconfined conditions and a small load (3 MPa) to improve the sample/transducer contact. A pair of stacked P-S<sub>1</sub>-S<sub>2</sub> 1.3 MHz transducers (ErgoTech) was located at the bottom (emitter) and top (receiver) of the plug. In order to check the anisotropy of the rock, 3 plugs cored in orthogonal directions were also extracted: one normal to bedding (Z) and two parallel to bedding (X and Y). Each one of these plugs was stepwise rotated ( $20^\circ$  increment).

The average P- and S- velocity in the Y-Z directions are 3.32 and 1.72 km/s, respectively. However the velocities obtained in the X direction are smaller (2.99 and 1.53 km/s). These low values suggest that porosity is not equally distributed (larger in the X-direction), what could obey to local changes in the cross bedding sets sampled by the X and Y plugs. The dynamic Young modulus and Poisson ratio computed from the previous velocities are  $15.90 \pm 0.06 \text{ GPa}$  and  $0.316 \pm 0.001$  (Y-Z directions) and  $12.55 \pm 0.11 \text{ GPa}$  and  $0.323 \pm 0.002$  (X direction). Static moduli, as expected, are lower than the dynamic ones because the latter only captures the elastic response of the rock under low stress conditions.

### Hydraulic Conductivity.

The hydraulic conductivity of the Corvicio Sandstone was tested in three 38.1 mm plugs sampled in the previously described orthogonal directions. The tests were conducted in a Hassler-type core holder (Temco THC) at different confining pressures (up to 30 MPa; fig. 3) and room T. In the tests, deaired tap water was injected (Quizix SP-5400 syringe pump) at a constant P while flow was measured at the outlet of the plug at 0.1 MPa. P and flow was carefully recorded with the Quizix system. Attainment of the steady flow condition while keeping injection P constant makes possible the computation of hydraulic conductivity based on Darcy's Law. Results show that the plug sampled in the X-direction has a higher conductivity than in the other two directions, which are similar. This is consistent with the observations made with P- and S- wave velocities. Significant hysteresis is observed when

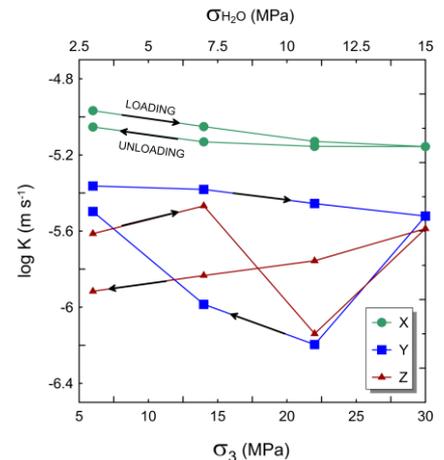


fig 3. Log hydraulic conductivity vs. confining ( $\sigma_3$ ) and pore ( $\sigma_{H_2O}$ ) pressures of three Corvicio Sandstone plugs sampled in orthogonal directions: X and Y parallel to bedding and Z at right angle.

considering loading/unloading stress paths, with lower conductivities in the unloading branch. Hysteresis is higher in the Y and Z directions. This behavior can be explained by the irreversible compaction of the samples.

### ACKNOWLEDGEMENTS.

Some of the determinations were performed at the esCO<sub>2</sub>-CIUDEN facilities and the Colorado School of Mines. Assistance and advice of Drs. T. Kovacs and M. Batzle are kindly acknowledged. Funds for this work have been provided by the XUGA Project 10REM003CT and the European Regional Development Funds 2007/2013

### REFERENCES.

- Hakala, M., Kuula, H., Hudson, J.A. (2007): Estimating the transversely isotropic elastic intact rock properties for in situ stress measurement data reduction: A case study of the Oikilouto mica gneiss, Finland. *Int. J. Rock. Mech. Min. Sci.*, **44**, 14-46.
- Hernández, J.M., Pujalte, V., Robles, S., Martín-Closas, C. (1999): División estratigráfica genética del Grupo Campóo (Malm-Cretácico Inferior, SW Cuenca Vascocantábrica). *Rev. Soc. Geol. España*, **12**, 377-396.
- Hoek, E., Brown, E.T. (1980): *Underground Excavations in Rock*. The Institute of Mining and Metallurgy. London, 527 p.
- Hoek, E., Carranza-Torres, C., Corkum, B. (2002): Hoek-Brown criterion-2002 edition. *Proc. NARMS-TAC Conference*, Toronto, 267-273.
- Nicksiar, M., Martin, C.D. (2012): Evaluation of methods for determining crack initiation in compression tests of low porosity rocks. *Rock Mech. Rock. Eng.*, **45**, 607-617